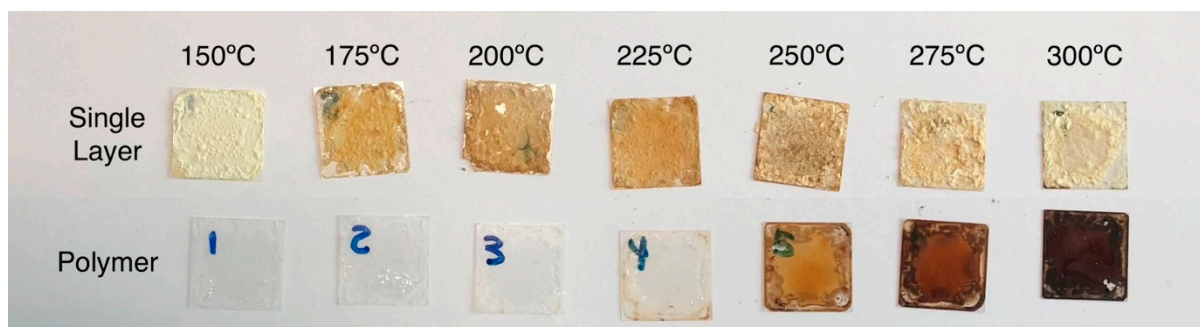
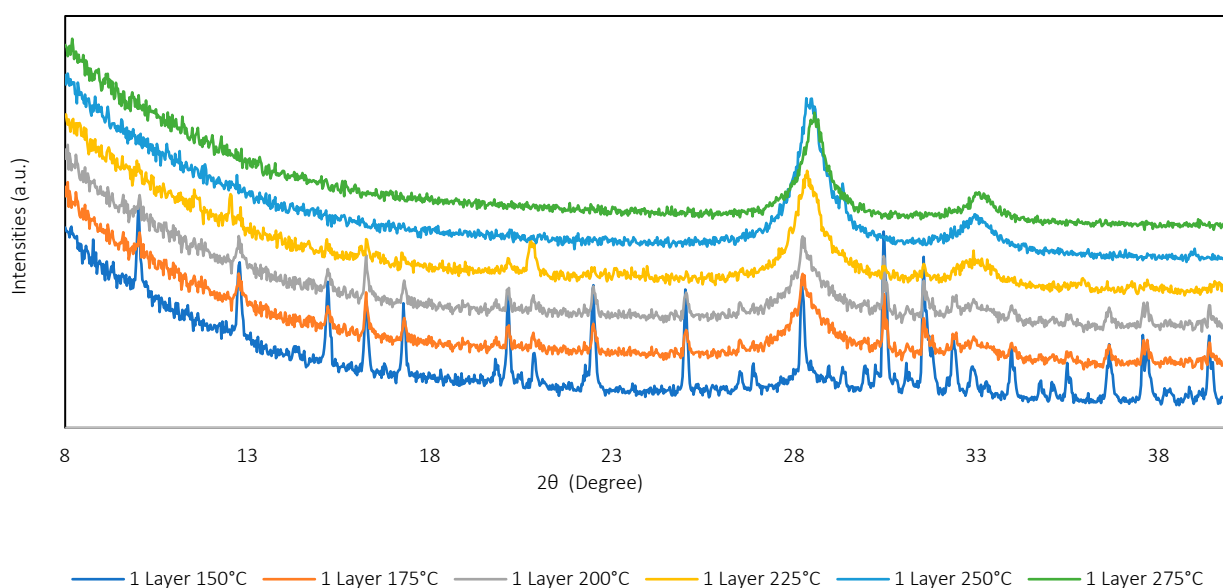


# The Effects of Irradiation on Structure and Leaching of Pure and Doped Thin-Film Ceria SIMFUEL Models Prepared via Polymer-Templated Deposition

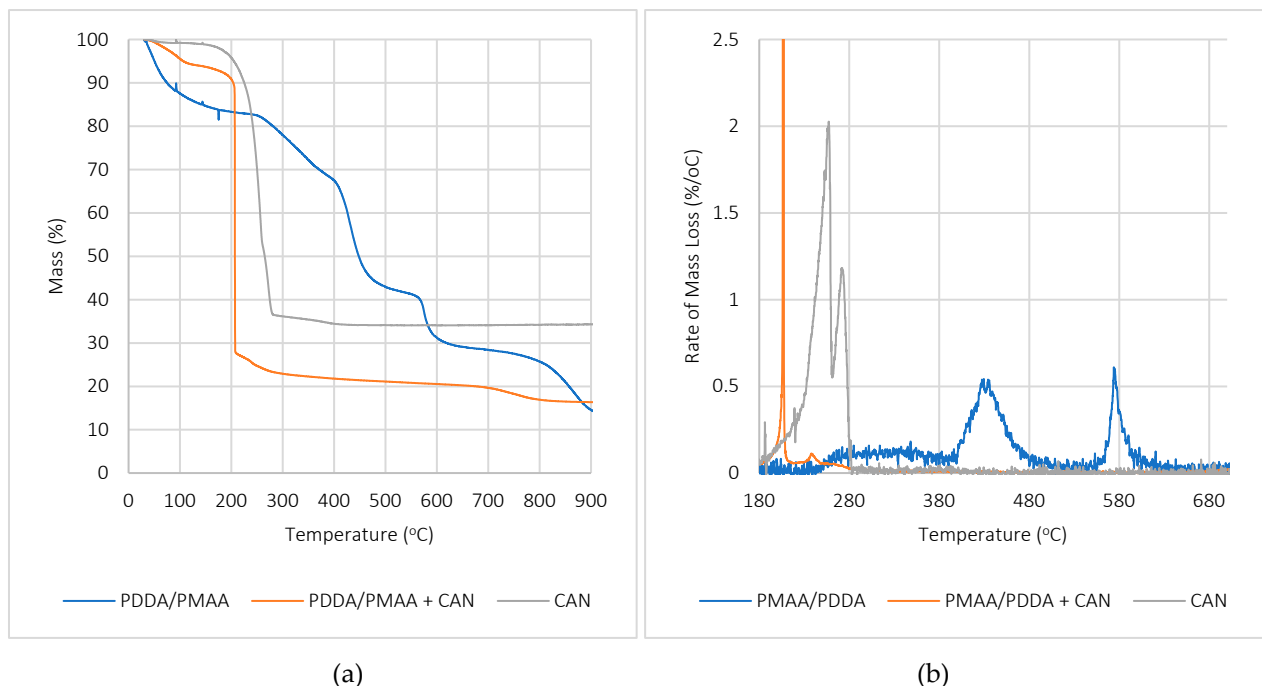


**Figure S1.** Effect of calcination temperature on deposited template and  $\text{CeO}_2$  films calcined under air for 30 mins. Above 200 °C, breakdown of the polymer template is observed alongside the onset of fragility in the  $\text{CeO}_2$ .

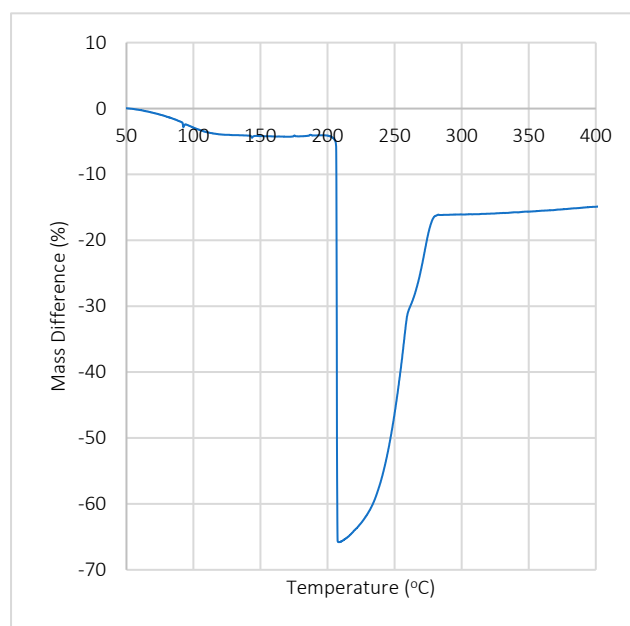


**Figure S2.** XRD diffraction patterns of films calcined at different temperatures for 30 mins, as outlined in **Figure S1**. The  $\text{CeO}_2$  phase is beginning to form by 200 °C, and hence a longer calcination period at this temperature was selected.

TGA/DTA analysis of the dried (4 g/L) PDDA/PMAA template, evaporated CAN solution (0.1 M), and a 50:50 mixture by precursor volume of these two components was conducted under air, with the mass loss and rate of mass loss curves shown in **Figure S3a** and **S3b** respectively. Additionally, differential mass analysis, allowing for the quantification of negative or positive interactions between the CAN and polymer template was also conducted, as shown in **Figure S4**. The data points for this were calculated as per **Equation 2** [1–3], adjusting the calculated TGA curve for the mass ratios of the components within the system.



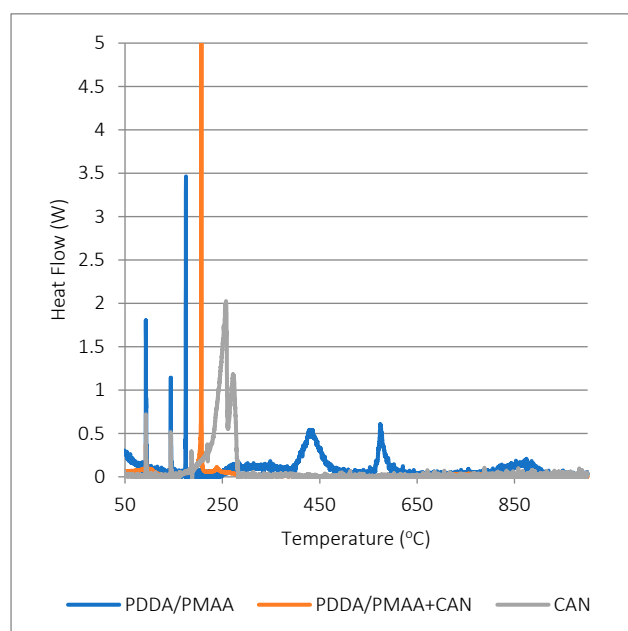
**Figure S3:** Mass loss curves (a), and rates of mass loss (b) for PDDA/PMAA polymer template, a combined sample, and CAN, as deposited. 100 mL.min<sup>-1</sup> air, 10 °C.min<sup>-1</sup>, ambient to 1000 °C. The peak mass loss rate of the combined sample is 114 wt%.°C<sup>-1</sup>. The associated heat flows accompanying these figures are presented in **Figure S5**.



**Figure S4.** Differential mass graph for the recorded TGA results, calculated as previously described. [1-3].

The degradation of the PMAA/PDDA template behaves in a similar way to the two separate components [4,5], and the small residue remaining at 1000 °C is likely NaCl. The PMAA/PDDA template is stable to 240 °C with no discernible mass loss following the loss of water by 200 °C. The onset of CAN degradation as measured here is *ca* 180 °C combined with a two-stage mass loss with peak rates of mass loss at 258 and 276 °C respectively, mirroring the work of Audebrand [6]. Any differences in thermogravimetric response are due to the differences in sample preparation between this prior work and that presented here.

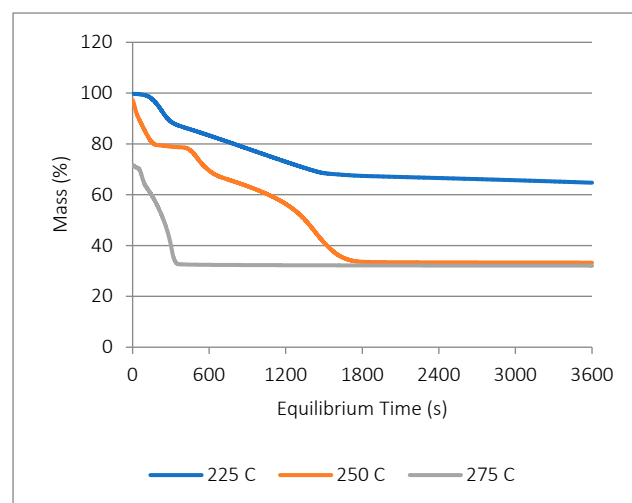
When combined, however, the thermal degradation of the PMAA/PDDA-CAN system is significantly altered, as illustrated by the large negative response shown in **Figure S4**. This illustrates a rapid evolution of volatiles at 207 °C, representing 66% of the mass if no interaction between the two components occurred. This coincides with a large DSC exotherm at the same temperature (see **Figure S1**). We can attribute this to a strong oxidative interaction between the Ce<sup>4+</sup> centres and/or nitrate functionalities of CAN and the polymer template, producing volatiles such as CO<sub>2</sub> (from oxidation of carboxylate functionalities) [5,7], and NO<sub>x</sub> (from nitrate decomposition), though confirmation of this would require TGA-FTIR, TGA-MS, or similar combinatorial analysis. This process likely mirrors the reactions intentionally utilised in nanoparticles combustion synthesis [7]. Above 280 °C, following the accelerated degradation observed in the combined sample, the observed mass is *ca* 15 wt% lower than would be expected in the absence of interactions. Thus, we can deduce that a sensible maximum calcination temperature for our films is 200 °C in this system to avoid undesired oxidation of the polymer template.



**Figure S5.** Heat flow of TGA data presented in **Figure S3**.

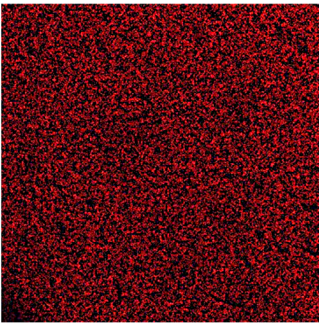


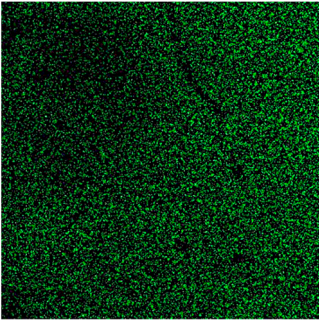
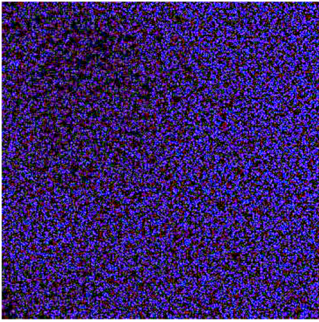
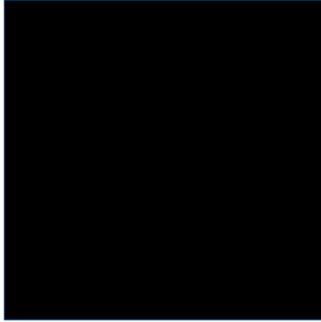
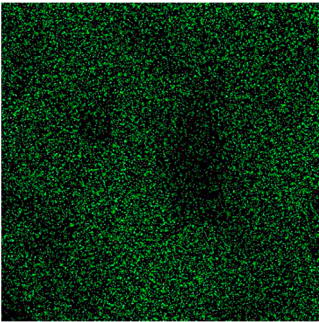

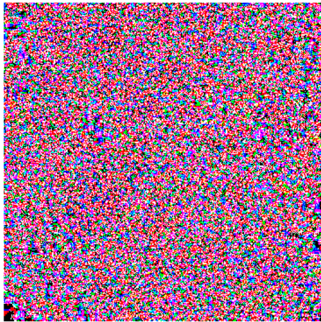
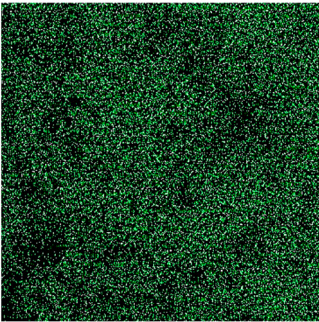
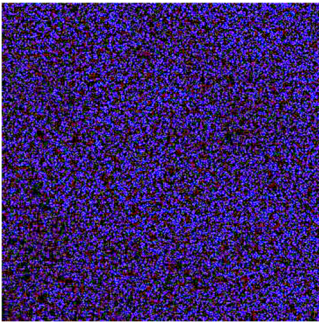
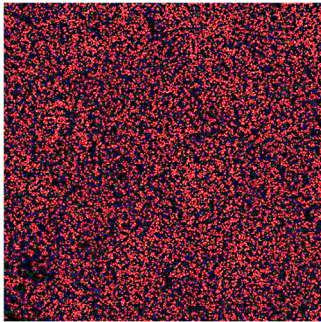


**Figure S6.** Photograph of slides after heating with varying time at 200 °C.

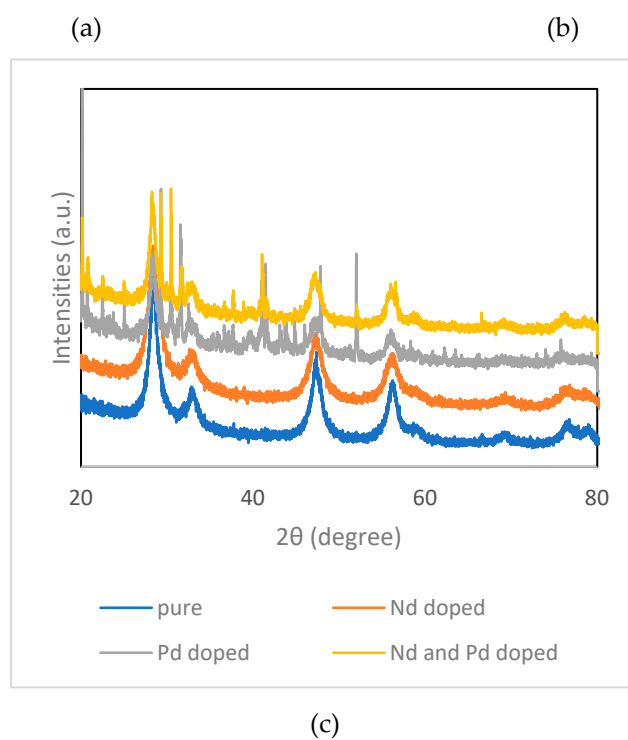
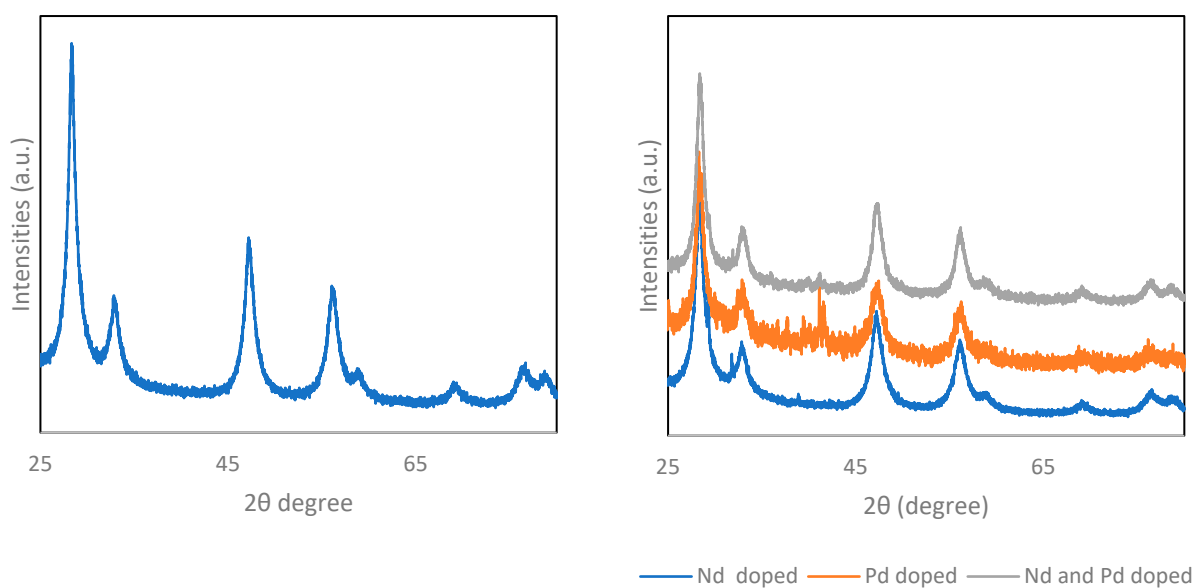


**Figure S7.** Variation in mass loss over time for pure CAN crystals held isothermally at a fixed temperature.

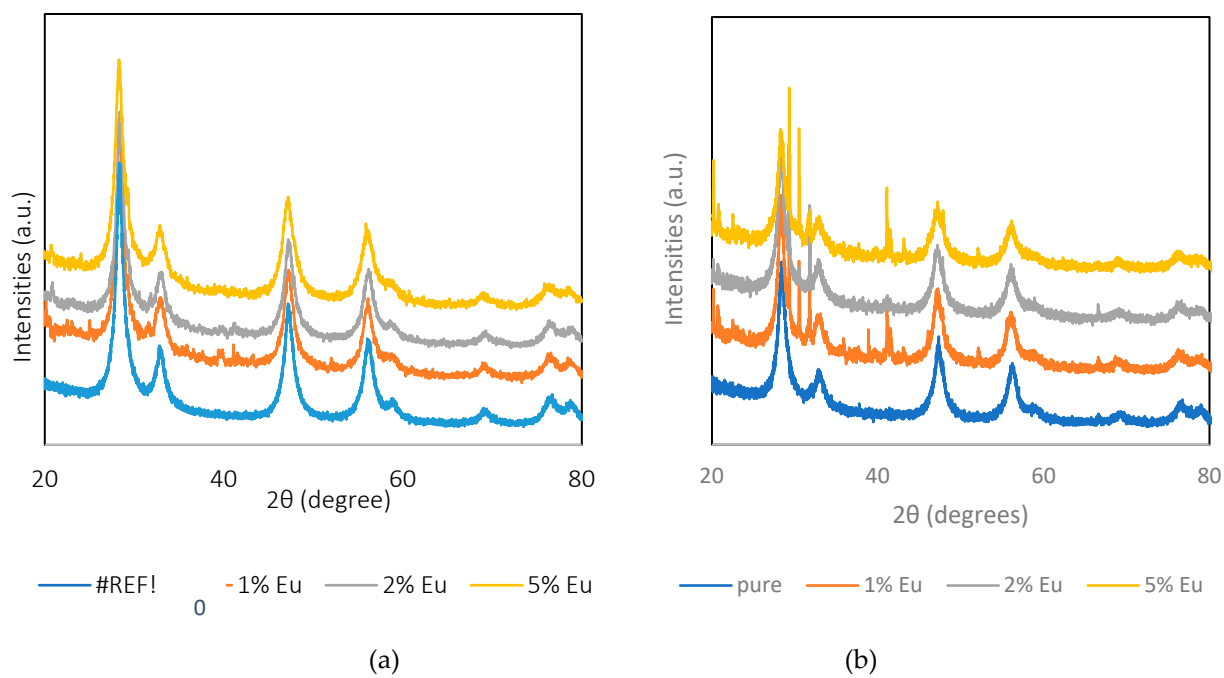


	Ce component	Nd component	Pd component
Pure CeO <sub>2</sub> film			
Nd doped CeO <sub>2</sub> film			
Pd doped CeO <sub>2</sub> film			
Nd and Pd doped CeO <sub>2</sub> film			

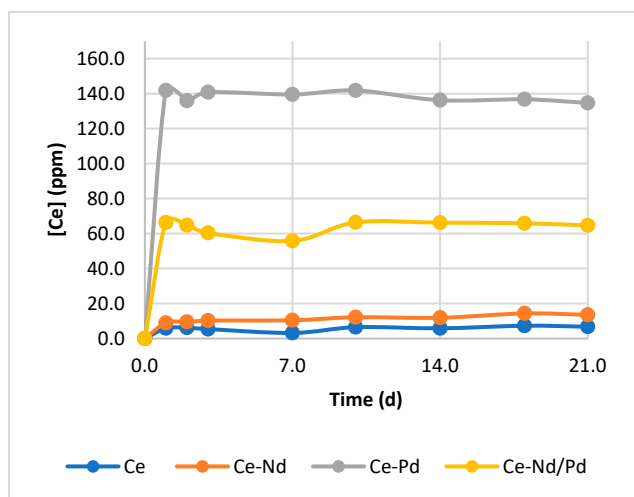
**Figure S8.** Elemental maps of pure CeO<sub>2</sub>, Nd, Pd, and Nd+Pd-doped films. The Eu-doped films were similarly homogenous. Full image width represents wide zoom of film surface – of the order of mm.



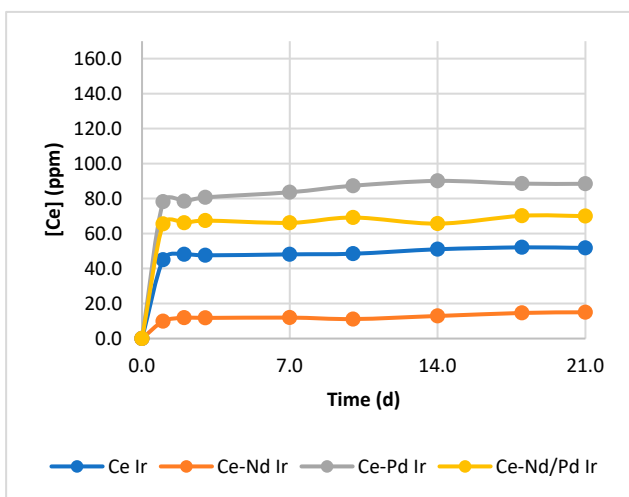
**Figure S9.** XRD Patterns of virgin (a –  $\text{CeO}_2$  and b –  $\text{Nd}$ ,  $\text{Pd}$ , and  $\text{Nd}+\text{Pd}$ -doped) and irradiated (c)  $\text{CeO}_2$  films.  $\text{Pd}$  elemental response visible (grey and yellow trace).  $\text{Pd}$  response increases upon irradiation.



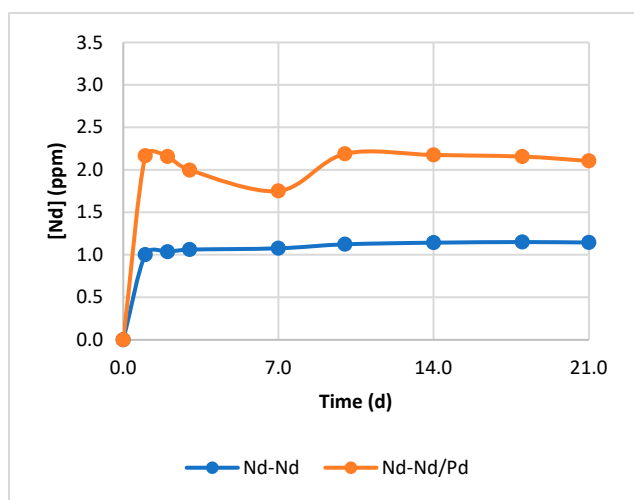
**Figure S10.** XRD Patterns of virgin (a) and irradiated (b) pure and Eu-doped  $\text{CeO}_2$  films. Note formation of nitratine ( $\text{NaNO}_3$ ) irradiation for 1% and 5% samples.



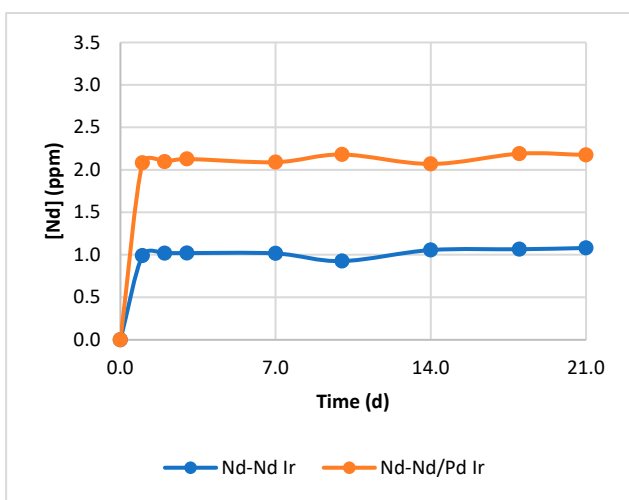
[a]



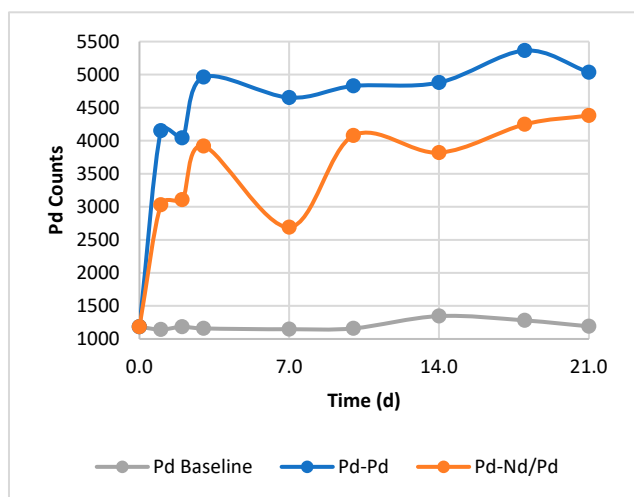
[b]



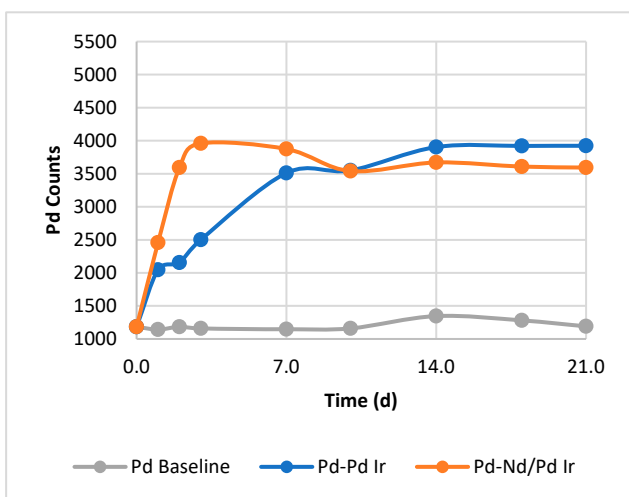
[c]



[d]



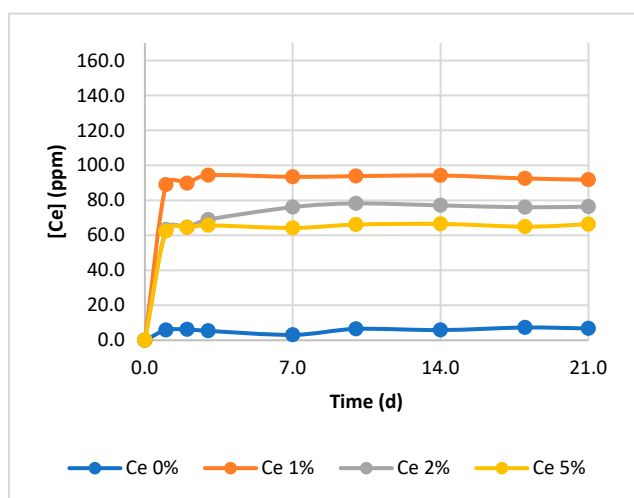
[e]



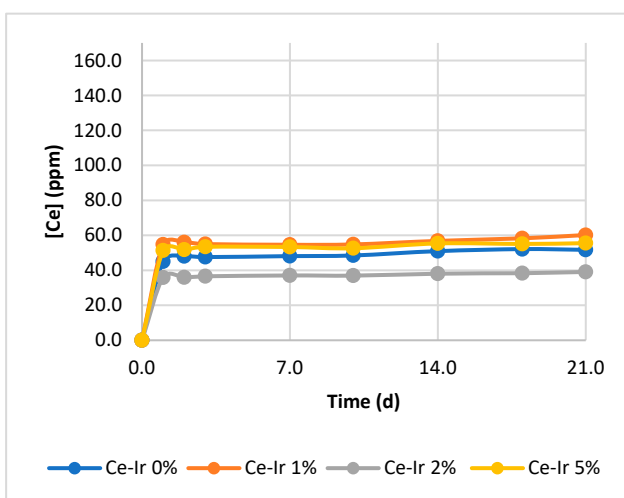
[f]

**Figure S11.** Ce (a and b), Nd (c and d), and Pd (e and f) leaching over time in Ce-Nd-Pd sample matrix. Virgin (a, c, e) and irradiated (Ir, b, d, f). The y-axis is scaled to the maximum concentration possible for each metal. 100% Ce: 168.13 ppm; 2% Nd: 3.46 ppm.

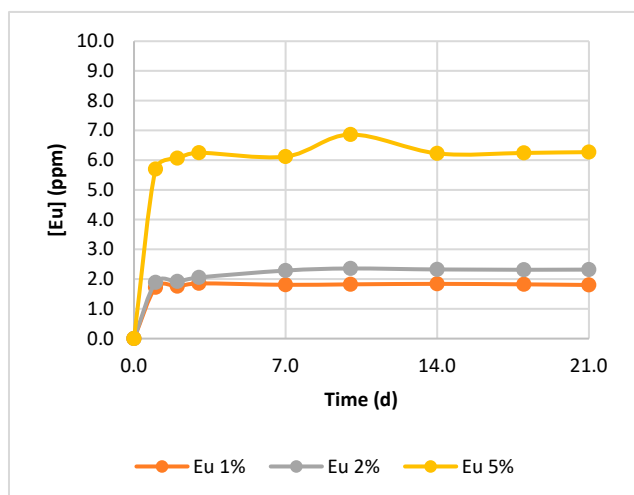




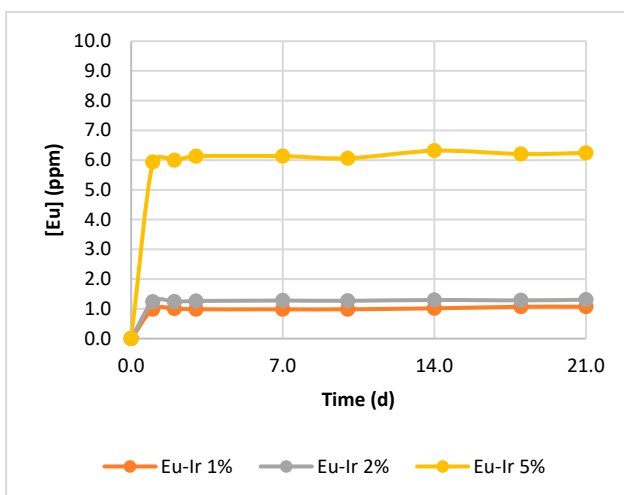
[a]



[b]

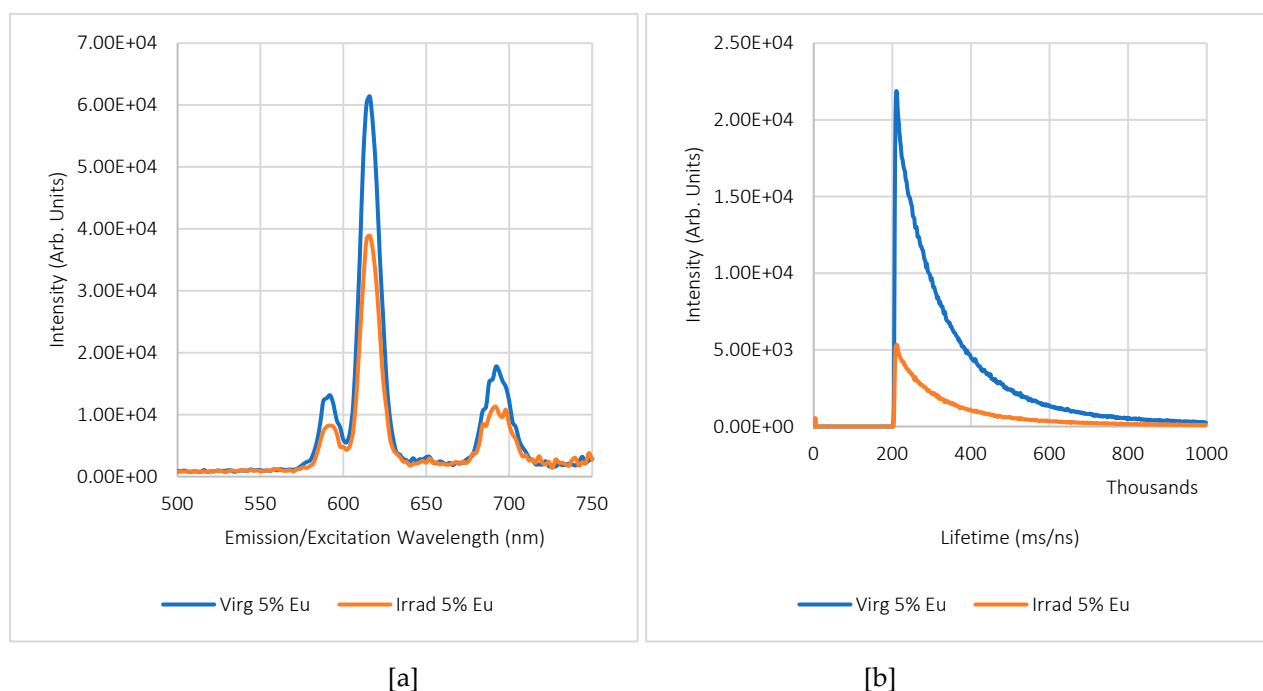


[c]



[d]

**Figure S12.** Ce (a and b), and Eu (c and d), leaching over time in Ce-Eu sample matrix. Virgin (a, c) and irradiated (b, d). The y-axis is scaled to the maximum concentration possible for each metal. Ce: 168.13 ppm; 1% Eu: 1.82 ppm; 2% Eu: 3.65 ppm; 5% Eu: 9.12 ppm.



**Figure S13.** TRLFS spectra of 5% Eu-doped virgin and irradiated CeO<sub>2</sub> films (a) with Eu lifetime (b).

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